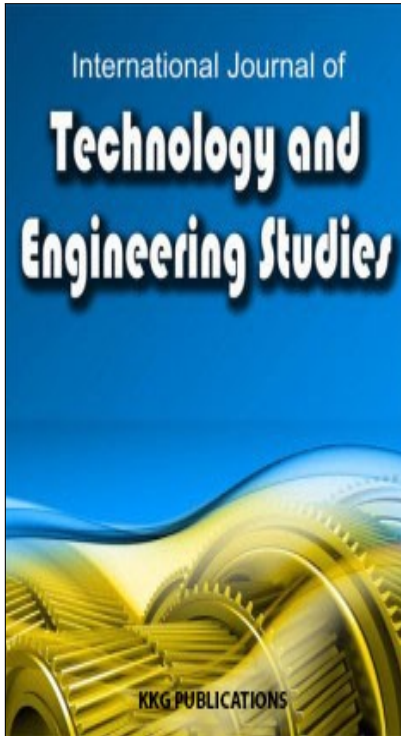
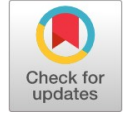


This article was downloaded by:
Publisher: KKG Publications



Key Knowledge Generation

Publication details, including instructions for author and subscription information:

<http://kkgpublications.com/technology/>

Non-Linear Fem-Based Shattering Simulation of Shelled Edible Agricultural Products: Walnut Shattering by Nut Cracker Hand Tool

H. KURSAT CELIK ¹, GOKHAN KUNT ², ALLAN E. W. RENNIE ³, IBRAHIM AKINCI ⁴

^{1,2,4} Faculty of Agriculture, Akdeniz University, Antalya, Turkey

³ Engineering Department, Lancaster University, Lancaster, UK

Published online: 15 April 2017

To cite this article: H. K. Celik, G. Kunt, A. E. W. Rennie and I. Akinci, “Non-linear fem-based shattering simulation of shelled edible agricultural products: Walnut shattering by nut cracker hand tool,” *International Journal of Technology and Engineering Studies*, vol. 3, no. 2, pp. 84-92, 2017.

DOI: <https://dx.doi.org/10.20469/ijtes.3.40006-2>

To link to this article: <http://kkgpublications.com/wp-content/uploads/2017/3/IJTES-40006-2.pdf>

PLEASE SCROLL DOWN FOR ARTICLE

KKG Publications makes every effort to ascertain the precision of all the information (the “Content”) contained in the publications on our platform. However, KKG Publications, our agents, and our licensors make no representations or warranties whatsoever as to the accuracy, completeness, or suitability for any purpose of the content. All opinions and views stated in this publication are not endorsed by KKG Publications. These are purely the opinions and views of authors. The accuracy of the content should not be relied upon and primary sources of information should be considered for any verification. KKG Publications shall not be liable for any costs, expenses, proceedings, loss, actions, demands, damages, expenses and other liabilities directly or indirectly caused in connection with given content.

This article may be utilized for research, edifying, and private study purposes. Any substantial or systematic reproduction, redistribution, reselling, loan, sub-licensing, systematic supply, or distribution in any form to anyone is expressly verboten.

NON-LINEAR FEM-BASED SHATTERING SIMULATION OF SHELLED EDIBLE AGRICULTURAL PRODUCTS: WALNUT SHATTERING BY NUT CRACKER HAND TOOL

H. KURSAT CELIK ^{1*}, GOKHAN KUNT ², ALLAN E. W. RENNIE ³, IBRAHIM AKINCI ⁴

^{1,2,4} Faculty of Agriculture, Akdeniz University, Antalya, Turkey

³ Engineering Department, Lancaster University, Lancaster, United Kingdom

Keywords:

Finite Element Method
Explicit Dynamics
Engineering Simulation
Compression Test
Walnut Fruit

Abstract. This paper presents a case study for non-linear Finite Element Method (FEM) based shattering simulation of shelled edible agricultural products. Walnut shell shattering using a simple nutcracker hand tool was considered in this case study. Some engineering properties were determined through physical compression tests to describe material models used in the FEM-based engineering simulation. Subsequently, a reverse engineering approach was employed in the solid modeling stage. The Walnut shell shattering case using a simple nutcracker hand tool was simulated considering non-linearity (explicit dynamics approach). Visual print-outs from simulation results revealed the shattering behavior of the walnut under defined boundary conditions. In addition to useful simulation print-outs of the shattering case, the time-dependent deformation behavior of the walnut during shattering was represented through charts. This work contributes to further research into the usage of non-linear numerical method-based deformation simulation studies for shelled edible agricultural products.

Received: 21 January 2017

Accepted: 12 March 2017

Published: 15 April 2017

INTRODUCTION

Walnut fruit is one of the oldest cultivated fruits in the world. The Walnut fruits kernel is consumed for its flavour and for nutritional reasons. It is a highly appreciated type of nut product because of its unique organoleptic characteristics and good sources of dietary fibre, various vitamins and minerals [1], [2]. They have garnered increased attention for their numerous health benefits. A considerable rise in production and consumer focus on walnut fruit has also been witnessed. The Food and Agriculture Organization of the United Nations (FAO) statistics indicate that the total production amount in the world in 2013 (FAOSTAT data May 2015) for Walnut fruit (kernel in shell) was 3,467,015.532 [tonnes], with the top five walnut producing countries being China (49.1%), Iran (13.1%), United States of America (12.1%), Turkey (6.1%) and Ukraine (3.3%). Most especially, consumers are paying more and more attention to the peeled Walnut kernel. To obtain the peeled kernel, a shelling operation is necessary. The shelling operation is the most critical and delicate step for achieving high quality kernels. Here, the mechanical properties of shelled agricultural products is a pre requisite for the design and development of cracking/shelling systems. Besides industrial shelling systems, domestic consumers use simple hand tools to extract the kernel. This is a basic compression process. In consideration of this, it is important to determine the mechanical properties and

deformation characteristics/behaviour of the walnut in order to progress optimally designed kernel extraction systems for both domestic users and industrial bulk production. This has provided the main motivation for the current simulations presented here. Another motivation is that there are many studies in the literature which are focused on predicting engineering properties and deformation/damage/failure characteristics of the agricultural/food products by means of linear FEM based simulation applications [3], [4], [5], [6], [7], [8], [9], [10], [11], [12], [13], [14], [15], [16], [17]. Consideration of the non linearity in these studies is absent or very limited. Non linearity can now be worked in FEM-based simulation codes efficiently. However, these types of non linear simulation have not yet become mainstream practice in research related to agricultural products' deformation.

The practical cases (such as the Walnut shell shattering issue in this paper) occurring in agricultural engineering mostly represent complex problems, which may be solved by numerical methods [18]. Nowadays, FEM is one of the popular numerical methods, which can be integrated to advanced computer aided technologies. FEM is a numerical method for solving engineering problems described by a set of partial differential equations and stress deformation field on the organic materials can be estimated using FEM with a good level of accuracy

*Corresponding author: H. Kursat Celik

†Email: hkcelik@akdeniz.edu.tr

[3], [19]. Here, it should be highlighted that understanding the structural deformation behaviour of shelled agricultural products is an important issue for high quality kernel extraction and this “know-how” would lead to well designed, efficient kernel extraction systems. In the literature, most of the studies are constructed on homogeneous linear elastic material model assumptions, considering deformation issues of agricultural products through implicit solvers with static loading conditions, however, the relationship between the loads and deformation may become non linear and at that point a non linear analysis should be undertaken in order to gain realistic results that reflect true-to-life behaviour. Non linearity can be divided into three aspects: Material models, (for example, hyper-elasticity, plastic flows, failure) (1); Contact conditions (for example, non linear contact conditions at high/low speed collisions and impact between elements) (2); and/or geometric deformation cases (for example, buckling and collapse) (3) [20]. The compression case can be described as a quasi static loading case with highly non linear contact conditions, especially in the case of compression of agricultural products. The explicit solution approach has proven valuable in solving quasi static problems, in addition to high velocity loading cases. The Explicit Dynamics system is designed to simulate non linear structural mechanics applications. In complicated applications, explicit methods are more applicable and the explicit approach provides an alternative problem-solving procedure. Therefore, it would not be wrong to say that deformation of the shelled agricultural products may be considered as non linear structural mechanics applications

covered by the explicit dynamics system mentioned above [21], [22], [23], [24]. As mentioned above, this paper introduces an explicit dynamics non-linear FEM-based deformation simulation case study for Walnut shell shattering using a simple nut cracker hand tool.

METHOD AND MATERIALS

Experimental Procedure

Physical compression tests were carried out for the Walnut (kernel-in-shell) and its kernel separately. Experimental procedures were set up in order to determine their physical deformation behaviour/characteristics and specific material properties such as modulus of elasticity, yield and fracture points. Some of these properties were also essential as input parameters in the simulation studies. Whole Walnut (kernel in shell) and sliced cubic kernel specimens (kernel specimen dimensions: 4x4x5 [mm]) were compressed between two rigid (relative to the product) plates. Three orientation loading scenarios were considered in whole walnut compression tests, namely longitudinal (Direction X), transverse (Direction Y) and suture (Direction Z) orientations. The Walnut type used in the tests were imported American Walnuts and they were collected from a commercial market shelf randomly in January 2016. All tests and measurements were carried out at the biological materials test laboratory of the Dept. of Agricultural Machinery and Tech. Engineering (Akdeniz University, Antalya, Turkey). A computer aided universal biological material test device (loading capacity: 2000 [N]) was utilised for the compression tests.

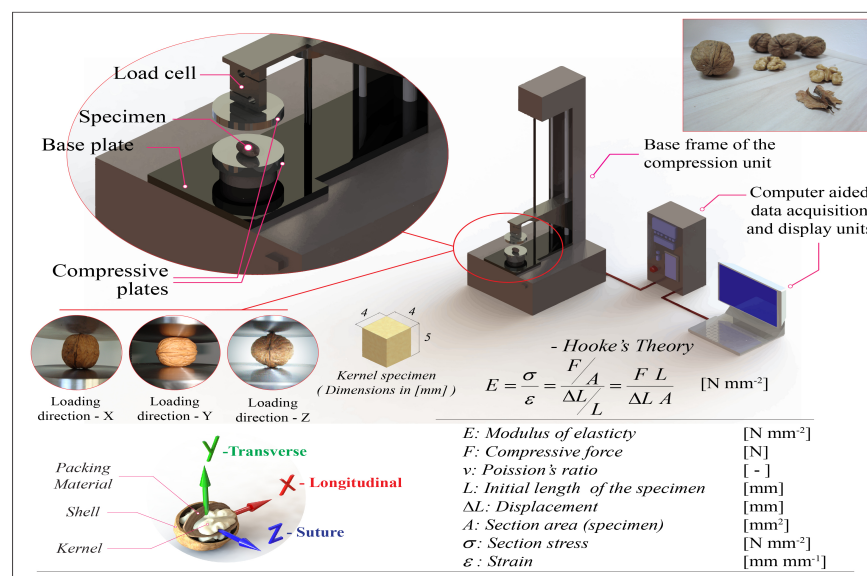


Fig. 1. Compression test setup

Tests were carried out for single moisture content of specimens ($6.86 \pm 0.22\%$ (w.b.)) at standard room temperature ($20\text{ }^{\circ}\text{C}$). Loading rate of $2.5\text{ [mm min}^{-1}\text{]}$ was set up for the tests to obtain precisely measured data (ASAE S368.4 W/Corr. 1 DEC 2000 (R2012)). The data sampling rate was 10 [Hz] . Ten

specimens for each of the tests were utilised in this experimental study. Experimental setup and graphical representation of the test results which exhibit the average force deformation characteristics of the Walnut (kernel in shell) and kernel specimens are shown in Fig. 1 and Fig. 2 respectively.

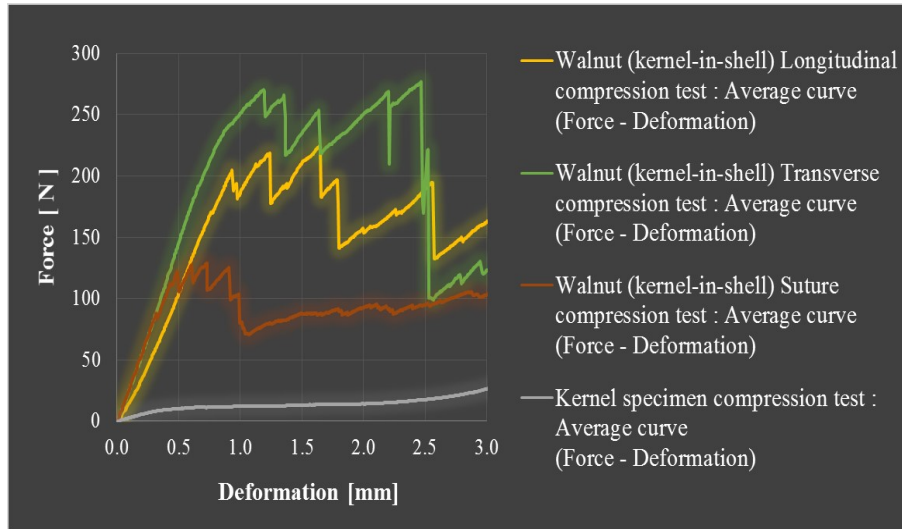


Fig. 2. Compression test results: Force Deformation characteristics average curves (Number of the specimens used in each of the tests: 10)

Material Model

True stress-strain data were converted from experimental force deformation data. They were used to calculate modulus of elasticity which is an essential property for determination of the deformation in the linear elastic loading stage of the materials [18], [25], [26], [27], [28], [29], [30]. Behind the elastic deformation, some problems may involve plastic deformation cases. Plastic deformation of the materials may be seen as a

material failure. In fact, it is valid for most organic materials. Plasticity is concerned with materials which initially deform elastically, but which deform plastically upon reaching a yield stress [31]. This phenomenon may also be seen in deformation of agricultural products. In this sense, the bi linear stress-strain relation under tensile and compression load can be drawn as shown in Fig. 3.

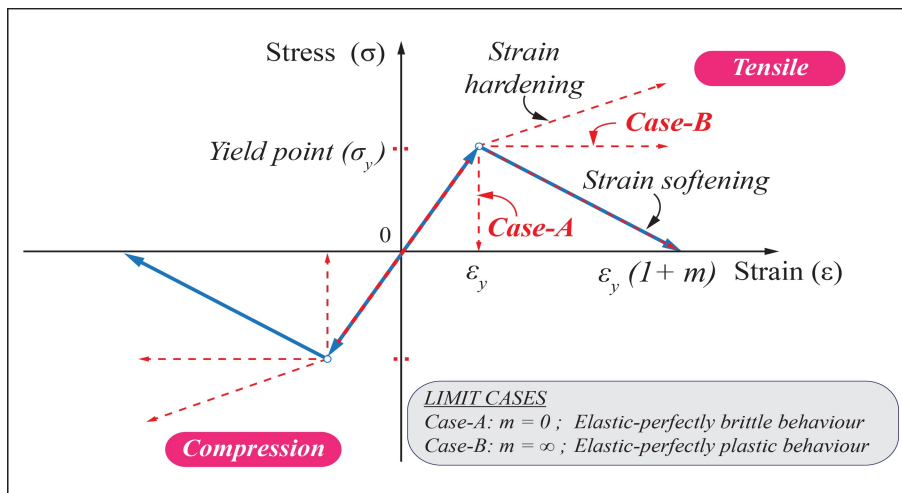


Fig. 3. Bi-linear stress-strain relation

Elastic perfectly brittle and bi linear strain hardening material deformation behaviours are described in Fig. 3, which are quite similar behaviours to the experimental deformation characteristics of the Walnut shell and kernel (Fig. 2) respectively. Hence, it would not be wrong to make assumptions of orthotropic perfectly brittle and elastic plastic (bi linear strain hardening) material models for Walnut shell and kernel respectively in a FEM-based simulation so that the deformation case can be simulated in a more realistic manner. Same material model was defined for packing material. The material model for the hand cracker tool was also assumed as an elastic plastic (bi linear strain hardening) material model (stainless steel

from FEM code’s non linear material library). In this regard, idealised material models and their properties can be described through experimental average true stress true strain curves of the Walnut shell and the kernel, as given in Fig. 4 and Table 1 respectively. Poisson’s ratio is another important parameter which is essential in deformation investigations of agricultural products. Poisson’s ratio has been studied for various agricultural products by a large number of researchers. Some of them consider the Poisson’s ratio values as 0.3 and 0.4 for shelled and soft/nut types of agricultural products respectively [12], [26], [32], [33], [34], [35], [36], [37], [38], [39], [40], [41], [42].

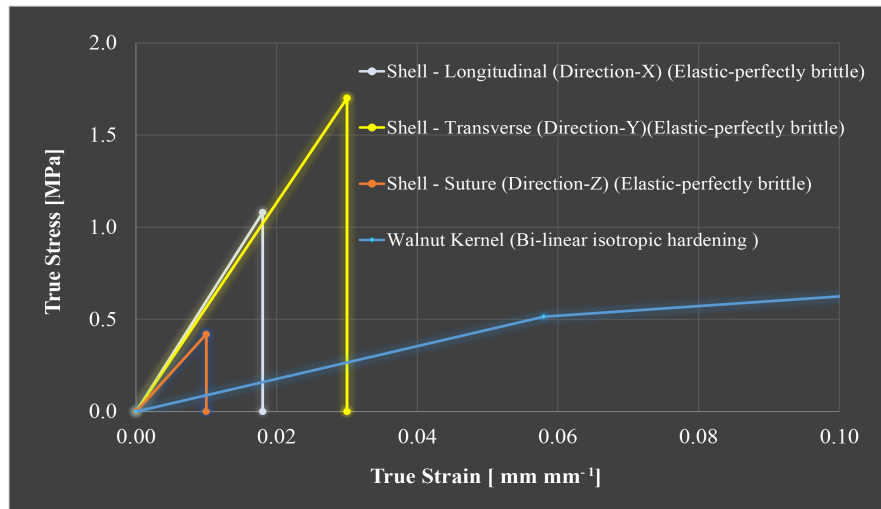


Fig. 4. Idealised Walnut shell and kernel material models used in FEM simulation (Orthotropic elastic perfectly brittle and bi-linear isotropic hardening models on experimental average true stress-true strain curve of the Walnut components)

TABLE 1
MATERIAL PROPERTIES

Material Properties	Shell (Longitudinal)	Shell (Transverse)	Shell (Suture)	Kernel	Stainless Steel
Modulus of Elasticity* [MPa]	63.916	71.783	42.770	9.335	193 x 10 ³
Tangent Modulus** [MPa]	-	-	-	2.235	1.8 x 10 ³
Yield Point (Damage) [MPa]	1.080	1.700	0.420	0.515	210
Force @ Yield Point [N]	162.640	229.574	83.707	7.770	-
Poisson’s Ratio [-]	0.30	0.30	0.30	0.40	0.31
Density [kg m ⁻³]	1044	1044	1044	958	7750

* Slope of the average true stress-strain curve in elastic region (tan α = modulus of elasticity)

**Slope of the average true stress-strain curve in plastic region (tan β =Tangent Modulus)

Non Linear FEM-Based Simulation Procedure

To obtain more realistic and accurate deformation results, a realistic description of the product geometry should be used in the structural analysis, because product geometry plays a

significant role in rheological investigations. One of the most useful methods of obtaining original/realistic digital Computer Aided Design (CAD) models of the organic materials with their complex surface forms is to use advanced Reverse Engineering

(RE) tools. In this work, the whole Walnut (kernel in shell) model was considered. The physical Walnut shell and kernel geometries were digitised using a Next Engine 3D desktop laser scanner. The scanning procedure was carried out for eight scanning sub-steps for the specimens in both vertical and horizontal positions. Macro range options with HD resolution was set up for the scanning process and total scanning time was 30 [min] approximately. SolidWorks 3D parametric solid modelling software features were used for ordering surface mesh structure and final surface refining operations of the product’s solid models. In addition, solid models of the Walnut components and a simple nut cracker hand tool design were realised specifically for this study.

In the non linear FEM simulation, a hand tool compression scenario in order to shatter the Walnut fruit (kernel in shell) was assumed. Explicit dynamics module of the ANSYS

Workbench commercial FEM code was utilised to simulate the scenario. Physical boundary conditions with frictional contact definition and idealized orthotropic elastic perfectly brittle and bi-linear isotropic hardening elastic-plastic material models were defined in the simulation setup. The bottom handle was fixed and the upper handle of the tool was employed to compress the Walnut fruit (kernel in shell).

An exaggerated loading rate of 2 [m s⁻¹] was assumed for upper plate compression in order to gain the physical solution time. The upper handle was compressed by 10 [mm]. Standard earth gravity (9.81 [m s⁻²]) was considered in the simulation. ANSYS Workbench advanced meshing functions with curvature meshing approach were used in creating the mesh structure of the product components. The simulation scenario, boundary conditions and mesh details of the models are demonstrated in Fig. 5.

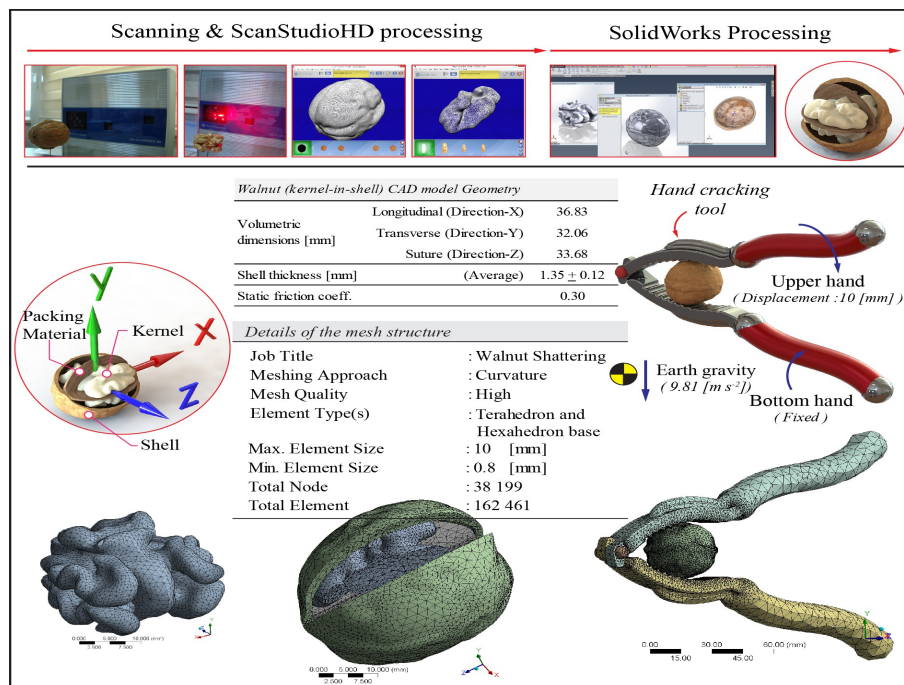


Fig. 5. Simulation set up

RESULTS AND DISCUSSION

After completion of the simulation solve time, the results were recorded. Visually, the simulation results extracted show logical physical deformation behaviour for the Walnut fruit and the hand tool under defined boundary conditions (Fig. 6). In addition to these useful visuals, numerical results based on the structural stress progression of the Walnut components, which are very complicated to obtain experimentally, were exhibited through data graphs.

Double axis chart A given in Fig. 6 demonstrates the maximum equivalent non linear stress deformation progression of the Walnut fruit components (whole fruit, shell and kernel) against time. Total simulation time was 0.005 [s]. Maximum equivalent stress values in this chart A were 5.370 [MPa] and 0.274 [MPa] for Walnut shell and kernel respectively. Whole Walnut (kernel in shell) stress progression can also be seen in this chart A. Stress progressions are considerably linear until a critical damage point for the shell is reached. Beyond these

points, stress progressions represent non linear progression against linear compression. The case of shattering was seen on the shell as a result of the stress progression being over the damage point of the shell material at many points during the compression action. Here, there can be seen differences in the stress progression between the shell and whole Walnut (kernel in shell). After deformation time of 0.002 [s] (approximately), the kernel started to make a contribution to the resistance against the compressive tool, which caused higher stress values for the whole walnut as is seen in the chart, however, the kernel deformation stayed within the linear deformation limits (dam-

age point: 0.515 [MPa]). It clearly indicates that there was no damage on the kernel: Damage-free kernel extraction. The other chart B represents stress deformation progression of the nut cracker hand tool against time. At first sight, maximum equivalent stress value of 288 [MPa] on the tool was beyond the defined yield point of the tool material (210 [MPa]). This indicated a plastic deformation failure on the tool. Geometry of the products under loading is a significant factor in deformation characteristics. This result highlights that a design change on the tool geometry should be realised.

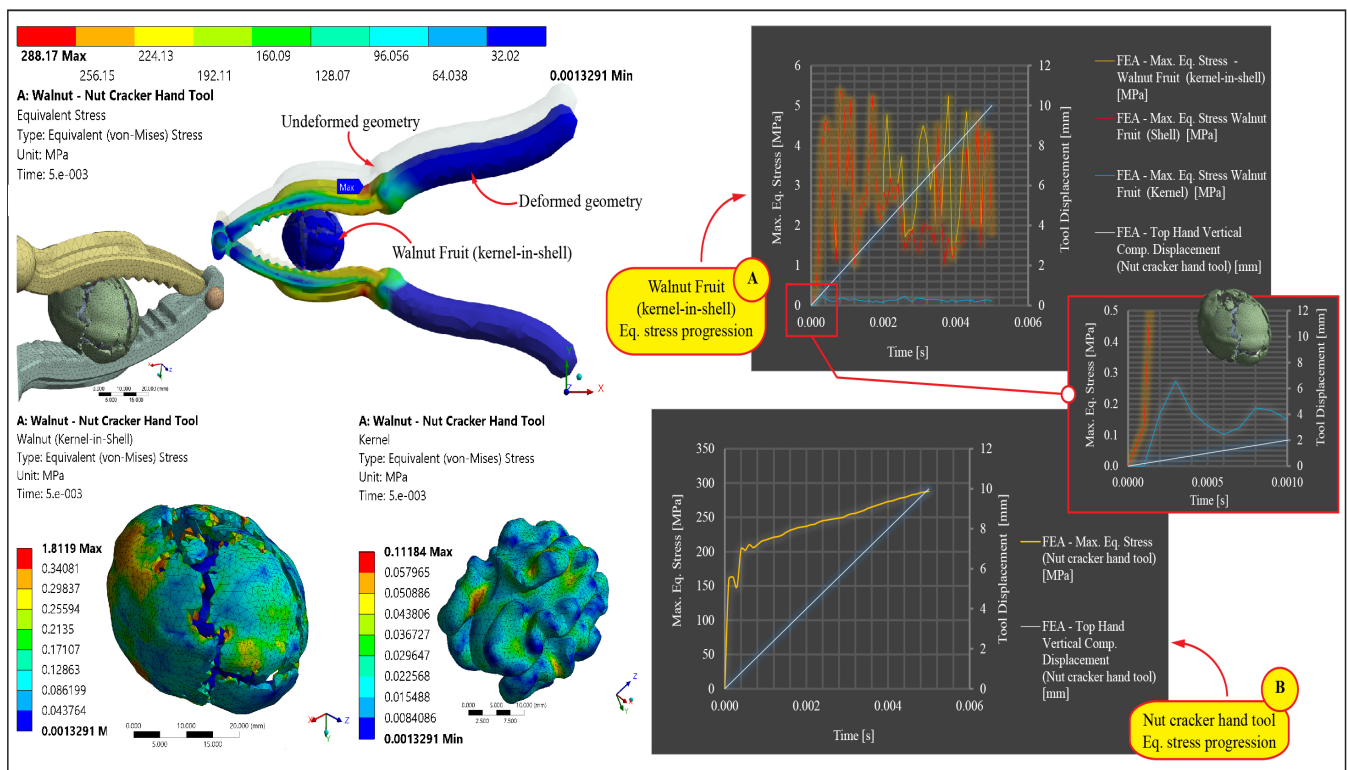


Fig. 6. Simulation results

CONCLUSION AND RECOMMENDATIONS

Mechanical kernel extraction method (basically applying compression) is one of the essential methods to extract kernels from shelled agricultural products without chemical processing. In this context, determination of the deformation characteristics of the target products under specific compression loading condition plays a significant role in the design of kernel extraction systems. Nowadays, technology allows for the realisation of productive, well designed mechanisation systems for efficient agricultural production phases. Most especially, advanced engineering simulation applications exhibit

great promise for efficient product processing and these applications will inevitably become mainstream practice in the design of the agricultural product processing industry. Some of the most important points extracted from this study can be summarised as follows:

1. Physical tests for the specimens revealed the force deformation characteristics of the Walnut fruit (kernel in shell) and kernel separately under compressive loading conditions and important mechanical properties were calculated through a converted stress-strain relationship as described by Hooke’s theory-based modulus of the elasticity calculation.

2. Physical tests for the specimens revealed that, although initial deformations were linear and elastic up to a critical point, brittle and plastic deformation cases were experienced beyond these critical points in the tests for Walnut shell and kernel respectively.

3. Experienced deformation cases were embedded into the material models which were used in the non linear time dependant FEM-based simulation procedure, and realistic compression simulations were accomplished as was intended. Simulation print outs exhibited logical physical deformation/characteristics.

4. Numerical results obtained from simulations also revealed that there were non linear changes in stress magnitudes against time during deformation. Maximum equivalent stress values were calculated as 5.370 [MPa], 0.274 [MPa] and 288 [MPa] for shell, kernel and the hand tool respectively.

5. Simulation results revealed plastic deformation failure on the nut cracker hand tool. This indicates that a design change could be necessary on the tool geometry for failure-free nut cracking operations.

One of the well known issues, which has affected the product deformation characteristics, is loading rate. Change of the loading rate may cause a different deformation response of the product under compression. In this study, a quick shattering case was considered in order to gain a physical simulation run-time. In future work, the focus may be on the loading rate effect on the deformation of Walnut fruit components under various loading rate conditions. This work contributes to further research into the usage of advanced numerical method-based engineering simulation studies for edible shelled agricultural products.

Declaration of Conflicting Interests

There are no associated conflicts of interest.

Acknowledgment

This work is partly supported financially by The Scientific Research Projects Coordination Unit of Akdeniz University (Turkey).

REFERENCES

- [1] S. M. T. Gharibzahedi, S. M. Mousavi, M. Hamed and F. Khodaiyan, "Engineering characterization of Persian walnut and its kernel (*Juglans regia* L.) for obtaining high quality produce," *Quality Assurance and Safety of Crops & Foods*, vol. 5, no. 2, pp. 145-156, 2013.
- [2] I. Das, N. G. Shah and G. Kumar, "Properties of walnut influenced by short time microwave treatment for disinfestation of insect infestation," *Journal of Stored Products Research*, vol. 59, pp. 152-157, 2014.
- [3] W. M. Cardenas and R. L. Strohshine, "Melon material properties and finite element analysis of melon compression with application to robot gripping," *Transactions of the ASAE*, vol. 34, no. 3, pp. 920-929, 1991.
- [4] H. Chen and J. De Baerdemaeker, "Modal analysis of the dynamic behavior of pineapples and its relation to fruit firmness," *Transactions of the ASAE*, vol. 36, pp. 1439-1444, 1993.
- [5] H. Chen and I. De Baerdemaeker, "Finite-element-based modal analysis of fruit firmness," *Transactions of the ASAE-American Society of Agricultural Engineers*, vol. 36, no. 6, pp. 1827-1834, 1993.
- [6] H. Chen, J. De Baerdemaeker and V. Bellon, "Finite element study of the melon for nondestructive sensing of firmness," *Transactions of the ASAE-American Society of Agricultural Engineers*, vol. 39, no. 3, pp. 1057-1058, 1996.
- [7] R. Lu and J. A. Abbott, "Finite element modeling of transient responses of apples to impulse excitation," *Transactions of the ASAE*, vol. 40, no. 5, pp. 1395-1406, 1997.
- [8] L. F. Hernandez and P. M. Belles, "A 3-D finite element analysis of the sunflower (*Helianthus Annuus* L.) fruit. Biomechanical approach for the improvement of its hullability," *Journal of Food Engineering*, vol. 78, no. 3, pp. 861-869, 2007.
- [9] O. Kabas, H. K. Celik, A. Ozmerzi and I. Akinci, "Drop test simulation of a sample tomato with finite element method," *Journal of the Science of Food and Agriculture*, vol. 88, no. 9, pp. 1537-1541, 2008.
- [10] H. K. Celik, O. Kabas, M. Topakci, A. Ozmerzi and I. Akinci, "Deformation behaviour simulation of a sample apple under the impact effect with finite elements method," in *International Congress on Mechanization and Energy in Agriculture*, Antalya, Turkey, pp. 893-897, Oct. 14-17, 2008.
- [11] A. Fabbri, C. Cevoli, E. Cocci and P. Rocculi, "Determination of the CO₂ mass diffusivity of egg components by finite element model inversion," *Food Research International*, vol. 44, no. 1, pp. 204-208, 2011.
- [12] H. Xu, S. Yan, Y. Wang and M. Liu, "Study on the walnut mechanical characteristics and shucking technology based on finite element analysis," in *International Conference on Computer and Computing Technologies in Agriculture*. Beijing,

- China, pp. 577-586, Oct. 29-31, 2011 .
- [13] C. C. Ihueze, C. E. Okafor and P. O. Ogbobe, "Finite design for critical stresses of compressed biomaterials under transportation," in *Proceedings of the World Congress on Engineering*, London, UK, July 3-5, 2013.
- [14] M. Petrua, O. Novakb, D. Herakc and S. Simanjuntakd, "Finite element method model of the mechanical behaviour of *Jatropha Curcas L.* seed under compression loading," *Biosystems Engineering*, vol. 111, no. 4, pp. 412-421, 2012.
- [15] H. A. Tinoco, D. A. Ocampo, F. M. Pena and J. R. Sanz-Urbe, "Finite element modal analysis of the fruit-peduncle of *Coffea arabica L.* var. Colombia estimating its geometrical and mechanical properties," *Computers and Electronics in Agriculture*, vol. 108, pp. 17-27, 2014.
- [16] S. Guessasma and H. Nouri, "Compression behaviour of bread crumb up to densification investigated using X-ray tomography and finite element computation," *Food Research International*, vol. 72, pp. 140-148, 2015.
- [17] A. Fabbri and C. Cevoli, "Rheological parameters estimation of non-Newtonian food fluids by finite elements model inversion," *Journal of Food Engineering*, vol. 169, pp. 172-178, 2016.
- [18] G. Sitkei, *Mechanics of Agricultural Materials*. New York, NY: Elsevier, 1987.
- [19] H. K. Celik, A. E. Rennie and I. Akinici, "Deformation behaviour simulation of an apple under drop case by finite element method," *Journal of Food Engineering*, vol. 104, no. 2, pp. 293-298, 2011.
- [20] Solid Works Documentation. (2010). *Solid works simulation premium: Nonlinear* [Online]. Available: <https://goo.gl/Xo8mXe>
- [21] N. Wakabayashi, M. Ona, T. Suzuki and Y. Igarashi, "Nonlinear finite element analyses: Advances and challenges in dental applications," *Journal of Dentistry*, vol. 36, no. 7, pp. 463-471, 2008.
- [22] H. H. Lee, *Finite Element Simulations with ANSYS Workbench 16*. Mission, KS: SDC Publications, 2015.
- [23] S. R. Wu and L. Gu, *Introduction to the Explicit Finite Element Method for Nonlinear Transient Dynamics*. Hoboken, NJ: John Wiley & Sons, 2012.
- [24] ANSYS Documentation. (2015). *Explicit dynamics analysis* [Online]. Available: <https://goo.gl/6HoR5n>
- [25] L. Shelef and N. N. Mohsenin, "Evaluation of the modulus of elasticity of wheat grain," *Cereal Chem*, vol. 44, no. 4, pp. 392-402, 1967.
- [26] N. N. Mohsenin, *Physical Properties of Plant and Animal Materials*. New York, Ny: Gordon and Breach, 1986.
- [27] J. Blahovec, "Mechanical properties of some plant materials," *Journal of Materials Science*, vol. 23, no. 10, pp. 3588-3593 1988.
- [28] J. Blahovec, "Strength and elasticity of some plant materials," in *International Conference Physical Properties of Agricultural Materials and their Influence on Technological Processes*, Rostock, Germany, pp. 60-66, Sept. 4-6, 1989.
- [29] R. L. Stroshine, *Physical Properties of Agricultural Materials and Food Products*. West Lafayette, IN: Purdue University Press, 2004.
- [30] C. C. Ihueze and C. E. Mgbemena, "Design for limit stresses of orange fruits (*Citrus sinensis*) under axial and radial compression as related to transportation and storage design," *Journal of the Saudi Society of Agricultural Sciences*, vol. 16, no. 1, pp. 72-81, 2015.
- [31] P. C. Pandey. (n.d.). *Continuum damage mechanics: Review of plasticity concepts, NPTEL-Civil engineering lecture notes, Module 4* [Online]. Available: <https://goo.gl/fK6RxX>
- [32] E. E. Finney, "The viscoelastic behaviour of the potatoe, *Solanum tuberosum*, under quasi-static loading," Ph.D. thesis, Michigan State University, East Lansing, MI, 1963.
- [33] C. H. Wang and Y. W. Mai, "Deformation and fracture of Macadamia nuts," *International Journal of Fracture*, vol. 69, no. 1, pp. 67-85, 1994.
- [34] E. Cakir, F. Alayunt and K. Ozden, "A study on the determination of Poisson's ratio and modulus of elasticity of some onion varieties," *Asian Journal of Plant Sciences*, vol. 1, no. 4, pp. 376-378, 2002.
- [35] M. Grotte, F. Duprat, E. Pietri and D. Loonis, "Young's modulus, Poisson's ratio, and Lamé's coefficients of golden delicious apple," *International Journal of Food Properties*, vol. 5, no. 2, pp. 333-349, 2002.
- [36] W. Burubai, E. Amula, R. M. Davies, G. W. W. Etekpe and S. P. Daworiye, "Determination of Poisson's ratio and elastic modulus of African nutmeg (*Monodora myristica*)," *International Agrophysics*, vol. 22, no. 2, pp. 99-102, 2008.
- [37] N. D. Patel, I. Grosse, D. Sweeney, D. S. Strait, P. W. Lucas, B. Wright and L. R. Godfrey, "An efficient method for predicting fracture of hard food source," in *ASME International Mechanical Engineering Congress and Exposition*, Boston, MA, pp. 521-528, Oct. 31-Nov. 6, 2008.

- [38] J. M. Boac, M. E. Casada, R. G. Maghirang and J. P. Harner III, "Material and interaction properties of selected grains and oilseeds for modeling discrete particles," *Transactions of the ASABE*, vol. 53, no. 4, pp. 1201-1216, 2010.
- [39] R. Khodabakhshian and B. Emadi, "Determination of the modulus of elasticity in agricultural seeds on the basis of elasticity theory," *Middle-East Journal of Scientific Research*, vol. 7, no. 3, pp. 367-373, 2011.
- [40] M. K. D. Kiani, H. Maghsoudi and S. Minaei, "Determination of Poisson's ratio and Young's modulus of red bean grains," *Journal of Food Process Engineering*, vol. 34, pp. 1573-1583, 2011.
- [41] R. Khodabakhshian, "Poisson's ratio of pumpkin seeds and their kernels as a function of variety, size, moisture content and loading rate," *Agricultural Engineering International: CIGR Journal*, vol. 14, no. 3, pp. 203-209, 2012.
- [42] G. Ipate, L. G. Ciulica and F. Rus, "Numerical modeling and simulation of cutting vegetable products," *INMATEH-Agricultural Engineering*, vol. 41, no. 3, pp. 5-10, 2013.

— This article does not have any appendix. —